

# CHAPTER 5

## Response and Stability Analysis in Frequency Domain

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# Chapter Outline

**5.1**

- Introduction to the concept of frequency response

**5.2**

- Introduction to simple open loop Bode plot

**5.3**

- Bode Plot - overall plotting

**5.4**

- Analysis of Bode Plot

# 5.1

## Introduction to the concept of frequency response

# The Concept

- Sinusoidal inputs to a linear system generate sinusoidal responses of the same frequency.
- However, they differ in amplitude and phase angle from the input.
- Sinusoids can be represented as complex numbers called *phasor*.

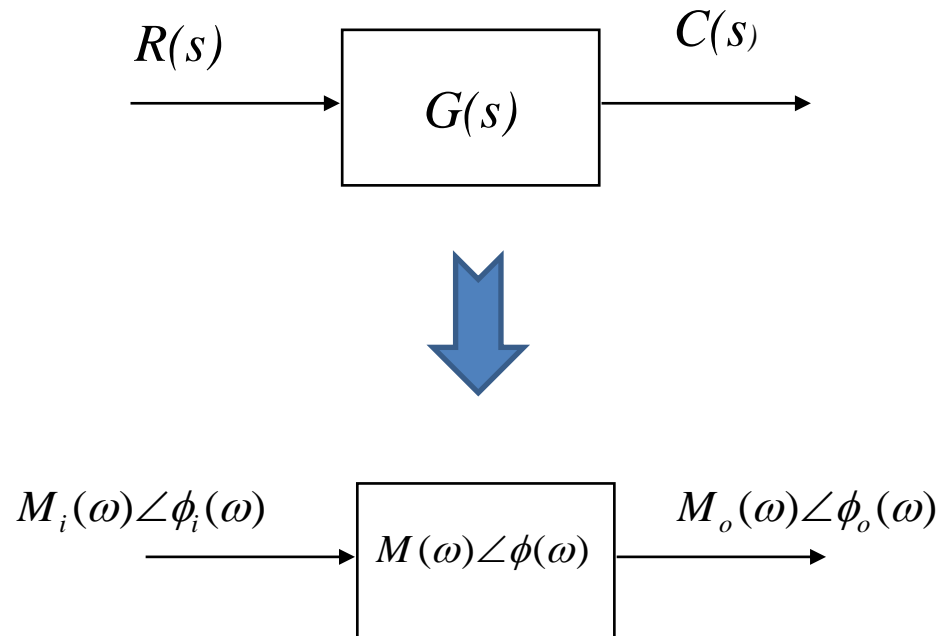
$$M_1 \cos(\omega t + \phi_1) = M_1 \angle \phi_1$$

where  $M_1$  and  $\phi_1$  are the amplitude and phase angle.

- Thus, the system can also be represented by a complex number so that the product of the input phasor and the system yield the phasor of the output.

# The Concept [2]

- The block diagram:



- The output sinusoid is found by multiplying the input and the system.

## The Concept [3]

Thus  $M_o(\omega) \angle \phi_o(\omega) = M_i(\omega) M(\omega) \angle [\phi_i(\omega) + \phi(\omega)]$

Magnitude frequency response  $M(\omega) = \frac{M_o(\omega)}{M_i(\omega)}$

Phase frequency response  $\phi(\omega) = \phi_o(\omega) - \phi_i(\omega)$

- The combination of the magnitude and phase frequency responses is called the **frequency response**,

$$M(\omega) \angle \phi(\omega)$$

- The frequency response of a system with transfer function  $G(s)$  is  $G(j\omega) = G(s) \Big|_{s \rightarrow j\omega}$

# Plotting Frequency Response

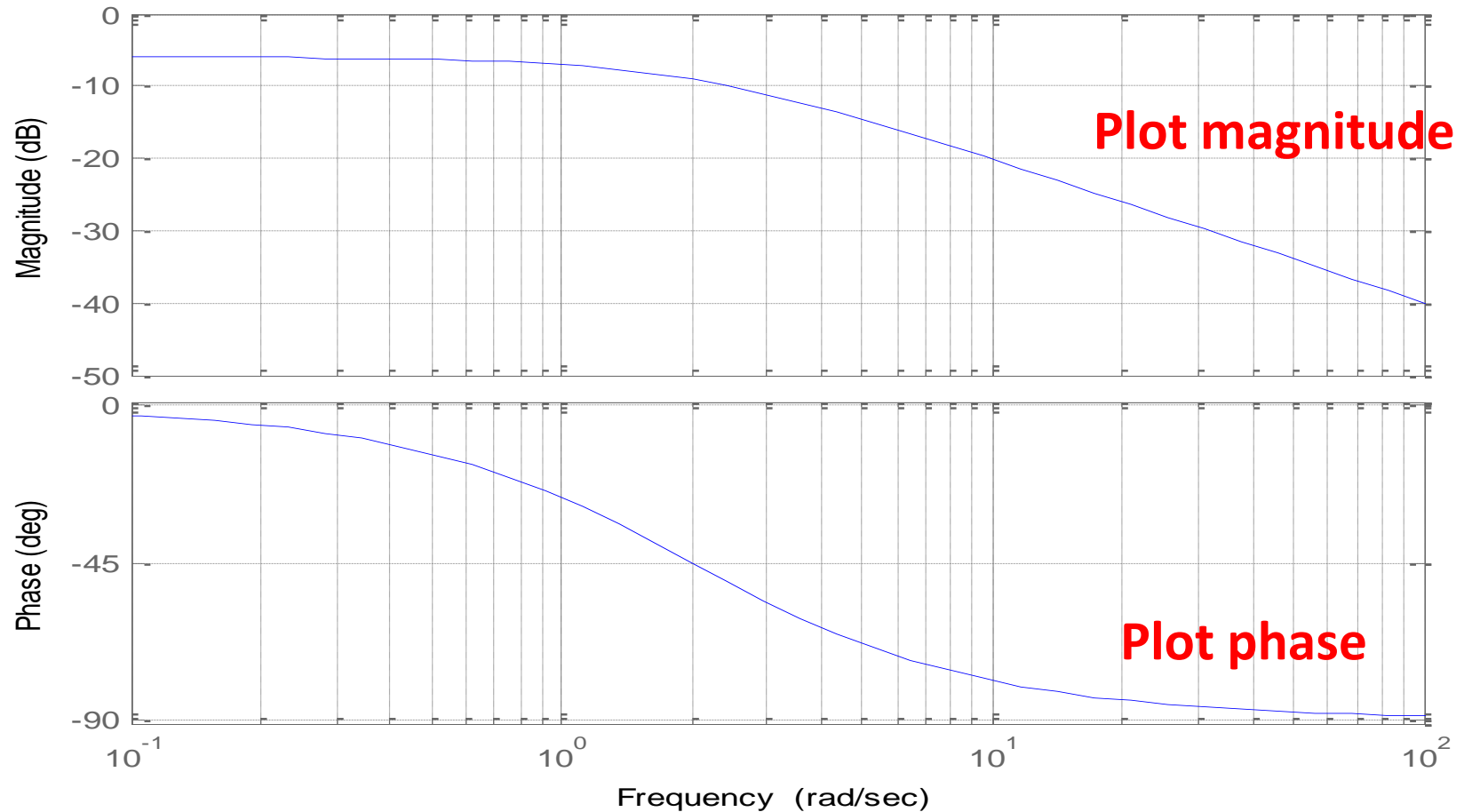
- For a given transfer function:  $G(s) = 1/(s+2)$

$$G(j\omega) = \frac{1}{(j\omega + 2)}$$

$$|G(j\omega)| = \frac{1}{\sqrt{(\omega^2 + 4)}}; \quad \phi(\omega) = -\tan^{-1}(\omega/2)$$

- One way to plot the Frequency response is by using a separate magnitude and phase plots.
  - Magnitude curve: decibel (dB) vs  $\log \omega$  [dB = 20 log M]
  - Phase curve: *phase angle vs log  $\omega$*

- Separate plots (magnitude and phase vs  $\log \omega$ ).





# 5.2

## Introduction to simple open loop Bode plot

## Bode Plots

- The log-magnitude and phase frequency response curves as a function of  $\log \omega$  is called **Bode plots**.
- Bode plot is a technique for analyses and design of control systems.

- Consider a transfer function 
$$G(s) = \frac{K(s + z_1)(s + z_2)\cdots(s + z_k)}{s^m(s + p_1)(s + p_2)\cdots(s + p_n)}$$

- The magnitude frequency response

$$|G(j\omega)| = \frac{K|(s + z_1)||s + z_2|\cdots|(s + z_k)|}{|s^m|(s + p_1)|(s + p_2)\cdots|(s + p_n)|} \Bigg|_{s \rightarrow j\omega}$$

- Converting into dB

$$\begin{aligned} 20\log|G(j\omega)| &= 20\log K + 20\log|(j\omega + z_1)| + 20\log|(j\omega + z_2)| + \cdots \\ &\quad - 20\log|(j\omega)^m| - 20\log|(j\omega + p_1)| - 20\log|(j\omega + p_2)| - \cdots \end{aligned}$$

## Bode Plots

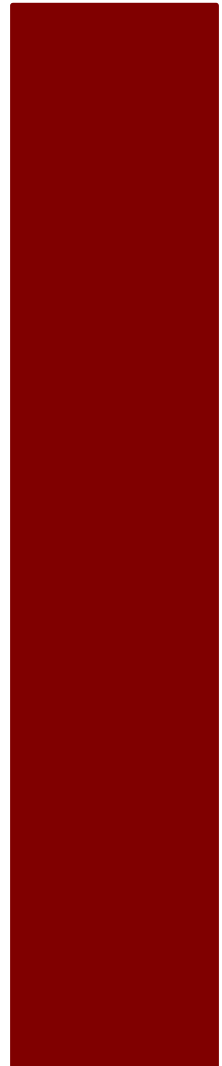
- The phase frequency response

$$\angle G(j\omega) = \angle K + \angle(j\omega + z_1) + \angle(j\omega + z_2) + \dots - \angle(j\omega + p_1) - \angle(j\omega + p_2) - \dots$$

- If we know the magnitude and phase responses of each term, total frequency response can be obtained by algebraic sum of each term.
- The frequency response can be simplified by utilizing straight-line approximations.
- Therefore, total frequency response can be obtained by graphic addition.

# 5.3

## Bode Plot – overall plotting



## Bode Plot

- Constant  $K$  :  $G(s)=K$
- Zeros at origin:  $G(s)=s$
- Poles at origin:  $G(s)=1/s$
- Zeros at real-axis ( $s$ -plane):  $G(s)=(s+a)$
- Poles at real axis ( $s$ -plane):  $G(s)= 1/(s+b)$

## Bode Plots - Constant $K$

- $G(s) = K$

$$G(s) = K; G(j\omega) = K$$

$$|G(j\omega)|_{dB} = 20\log K$$

$$\angle G(j\omega) = 0^\circ$$

## Bode Plots - Zeros at origin

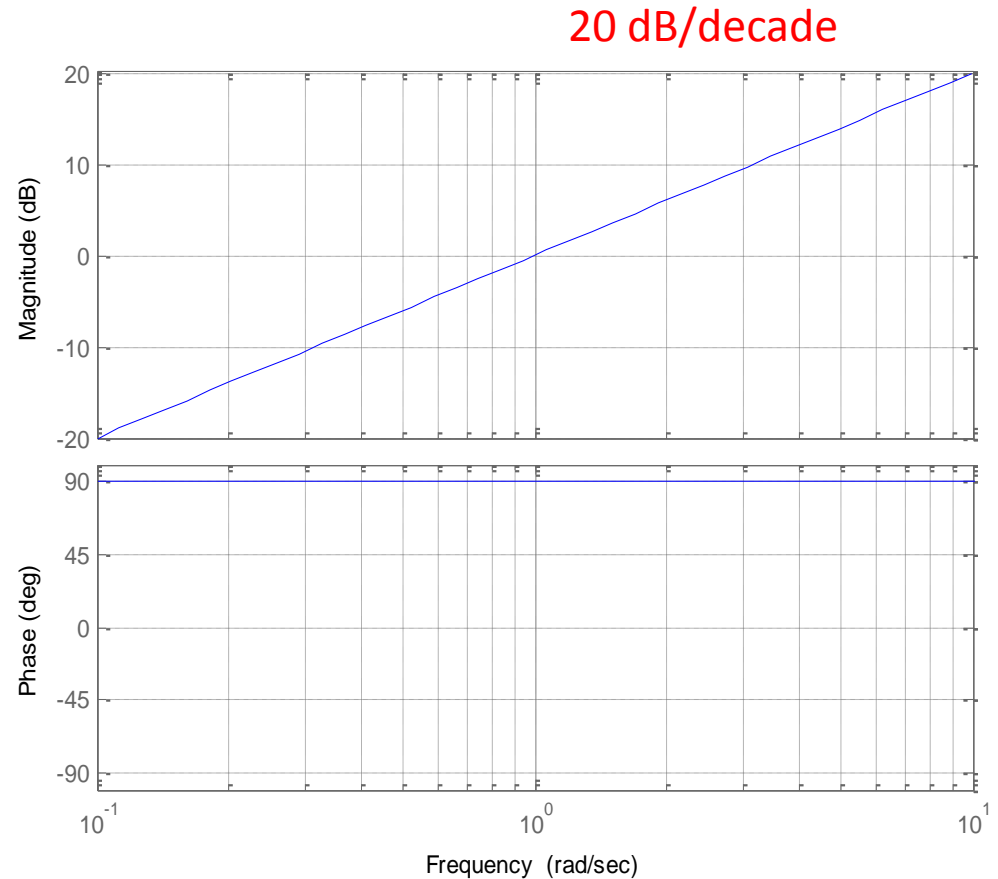
- $G(s) = s$  (Zero at origin)

$$G(s) = s; G(j\omega) = j\omega$$

$$|G(j\omega)|_{dB} = 20 \log \omega$$

$$\angle G(j\omega) = 90^\circ$$

- At  $\omega = 1$ , gain = 0 dB.



## Bode Plots- Poles at origin

- $G(s) = 1/s$  (pole at origin)

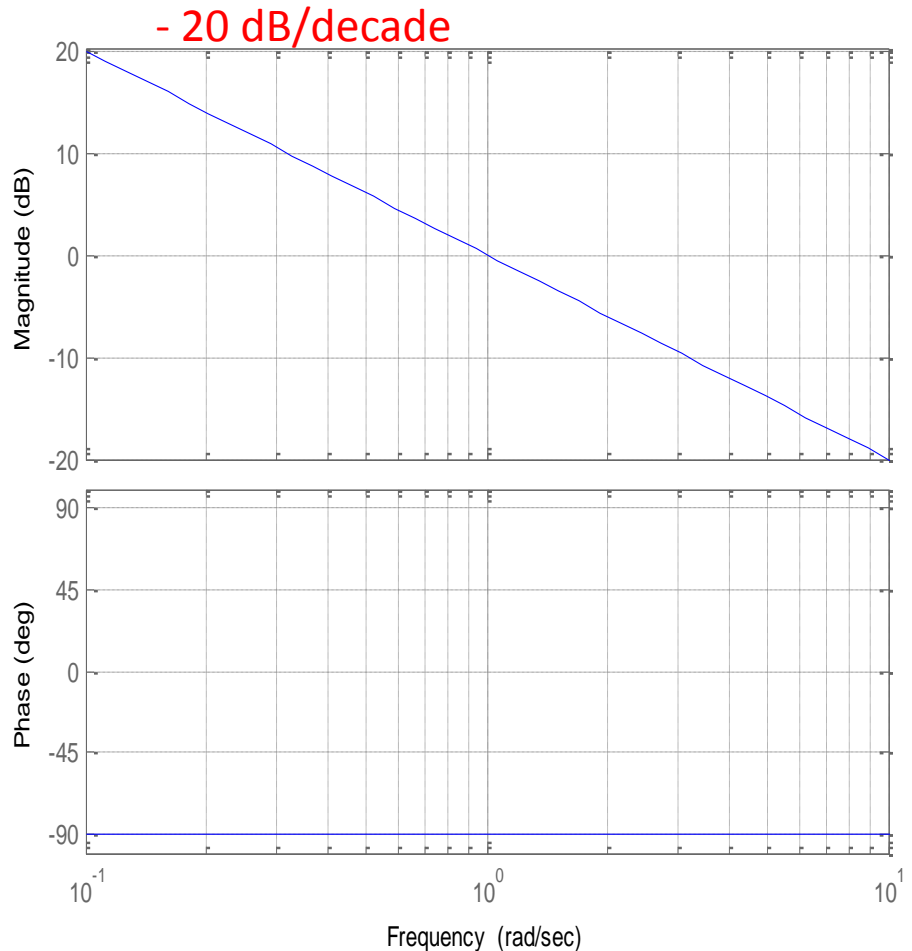
$$G(s) = 1/s; G(j\omega) = 1/j\omega$$

$$|G(j\omega)| = \log(1/\omega)$$

$$|G(j\omega)|_{dB} = 20\log(1/\omega) = -20\log \omega$$


$$\angle G(j\omega) = -90^\circ$$

- At  $\omega = 1$ , gain = 0 dB.





## Bode Plots – Zeros at real axis

• For  $G(s) = \frac{s}{a} + 1$    $G(s) = \left(\frac{s}{a} + 1\right); G(j\omega) = \frac{j\omega}{a} + 1$

$$|G(j\omega)| = \sqrt{\left(\frac{\omega}{a}\right)^2 + 1}$$

$$\angle G(j\omega) = \tan^{-1}\left(\frac{\omega}{a}\right)$$

• At  $\omega \ll a$ ,

$$|G(j\omega)|_{dB} = 20\log 1 = 0dB$$

$$\angle G(j\omega) = \tan^{-1} 0 = 0^\circ$$

• At  $\omega = a$ ,

$$|G(j\omega)|_{dB} = 20\log \sqrt{2} = 3.01dB$$

$$\angle G(j\omega) = \tan^{-1} 1 = 45^\circ$$

• At  $\omega \gg a$ ,

$$|G(j\omega)|_{dB} = 20\log \omega \quad \text{20 dB/decade}$$

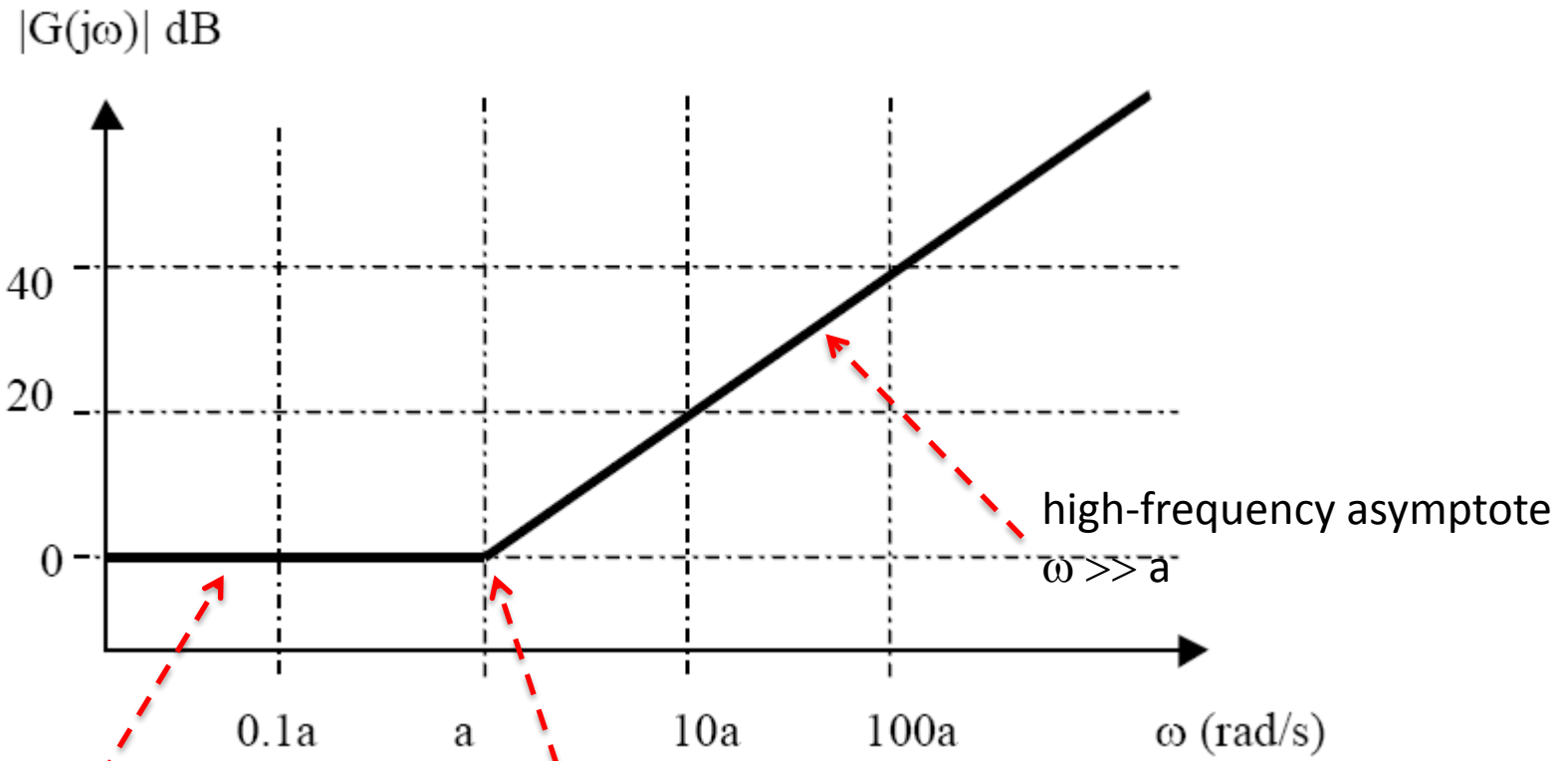
$$\angle G(j\omega) = \tan^{-1} \omega = 90^\circ$$

➤ The low-frequency approximation is called *the low-frequency asymptote*.

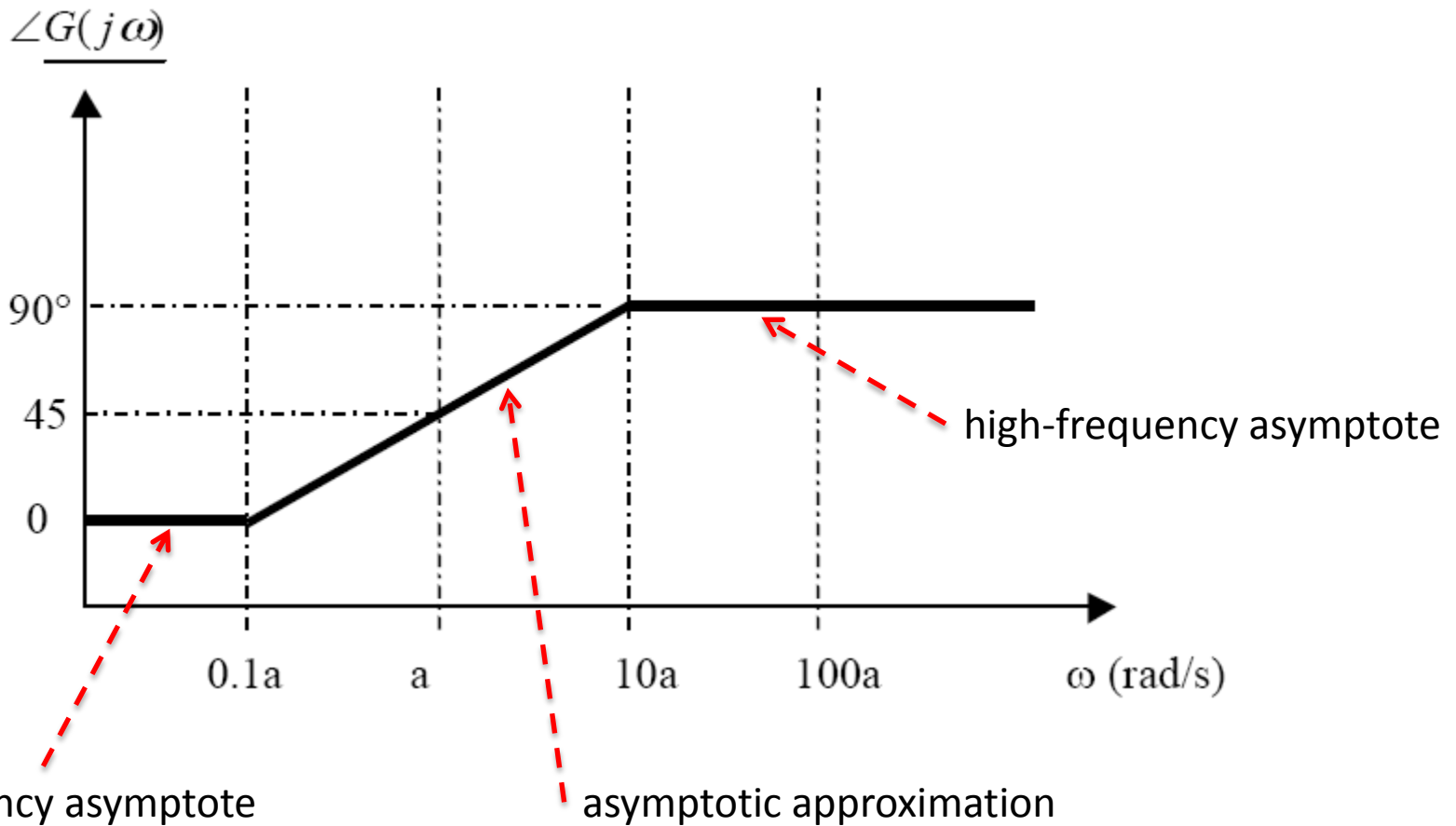
➤ The frequency,  $\omega = a$  is known as *break frequency* because it is the break between the low- and high-frequency asymptotes.

➤ The high-frequency approximation is called *the high-frequency asymptote*.


# Bode Plot- magnitude plot (Zeros)



# Bode Plot- Phase plot (Zeros)



## Bode Plots – Poles at real axis

- For  $G(s) = \frac{1}{\frac{s}{a} + 1}$    $G(s) = \left( \frac{1}{s/a + 1} \right); G(j\omega) = \left( \frac{1}{j\omega/a + 1} \right)$   
 $|G(j\omega)| = \frac{1}{\sqrt{\left(\frac{\omega}{a}\right)^2 + 1}}; \angle G(j\omega) = -\tan^{-1}\left(\frac{\omega}{a}\right)$

- At  $\omega \ll a$ ,

$$|G(j\omega)|_{dB} = 20 \log 1 = 0dB$$

$$\angle G(j\omega) = \tan^{-1} 0 = 0^0$$

- At  $\omega = a$ ,

$$|G(j\omega)|_{dB} = 20 \log(1/\sqrt{2}) = -3.01dB$$

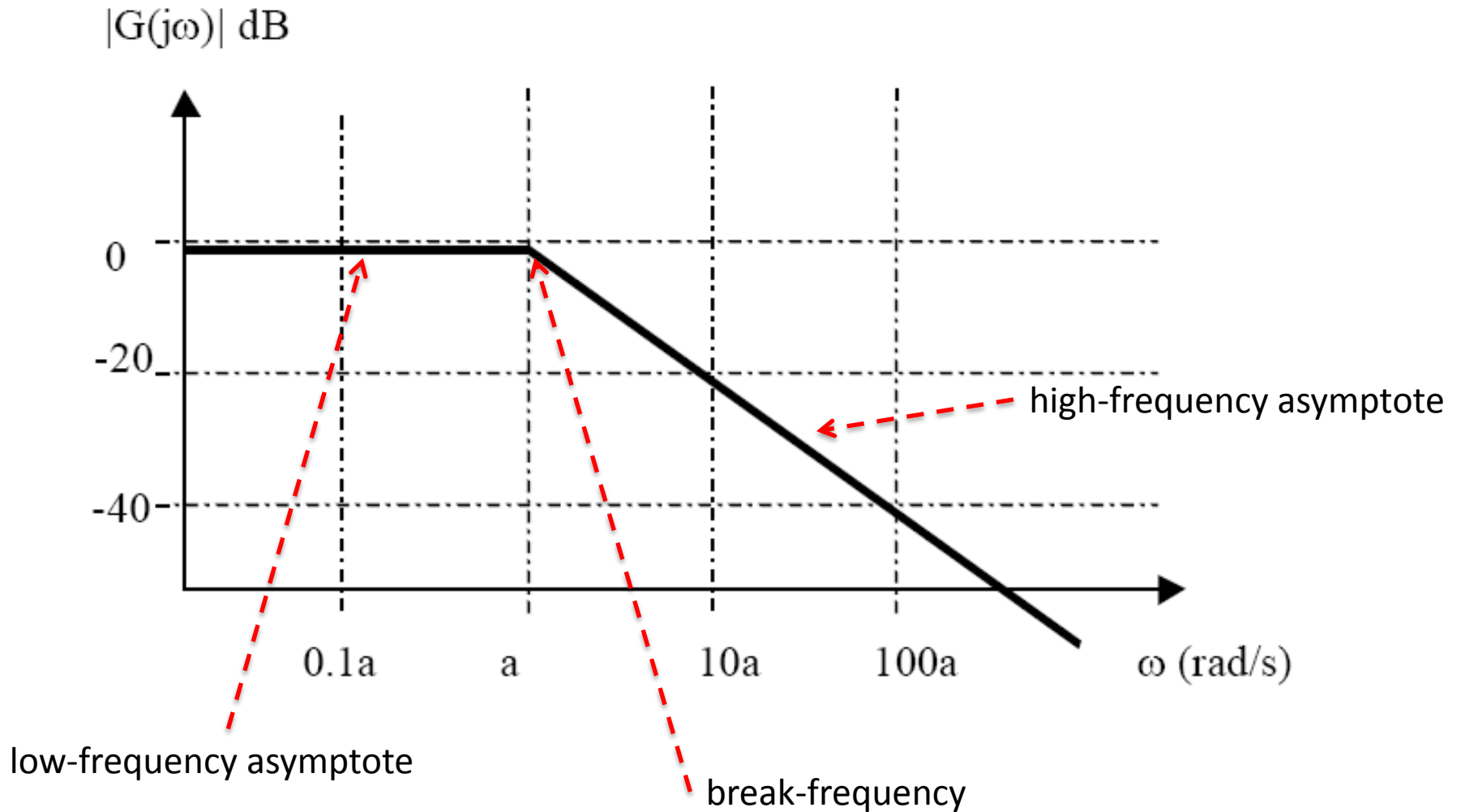
$$\angle G(j\omega) = -\tan^{-1} 1 = -45^0$$

- At  $\omega \gg a$ ,

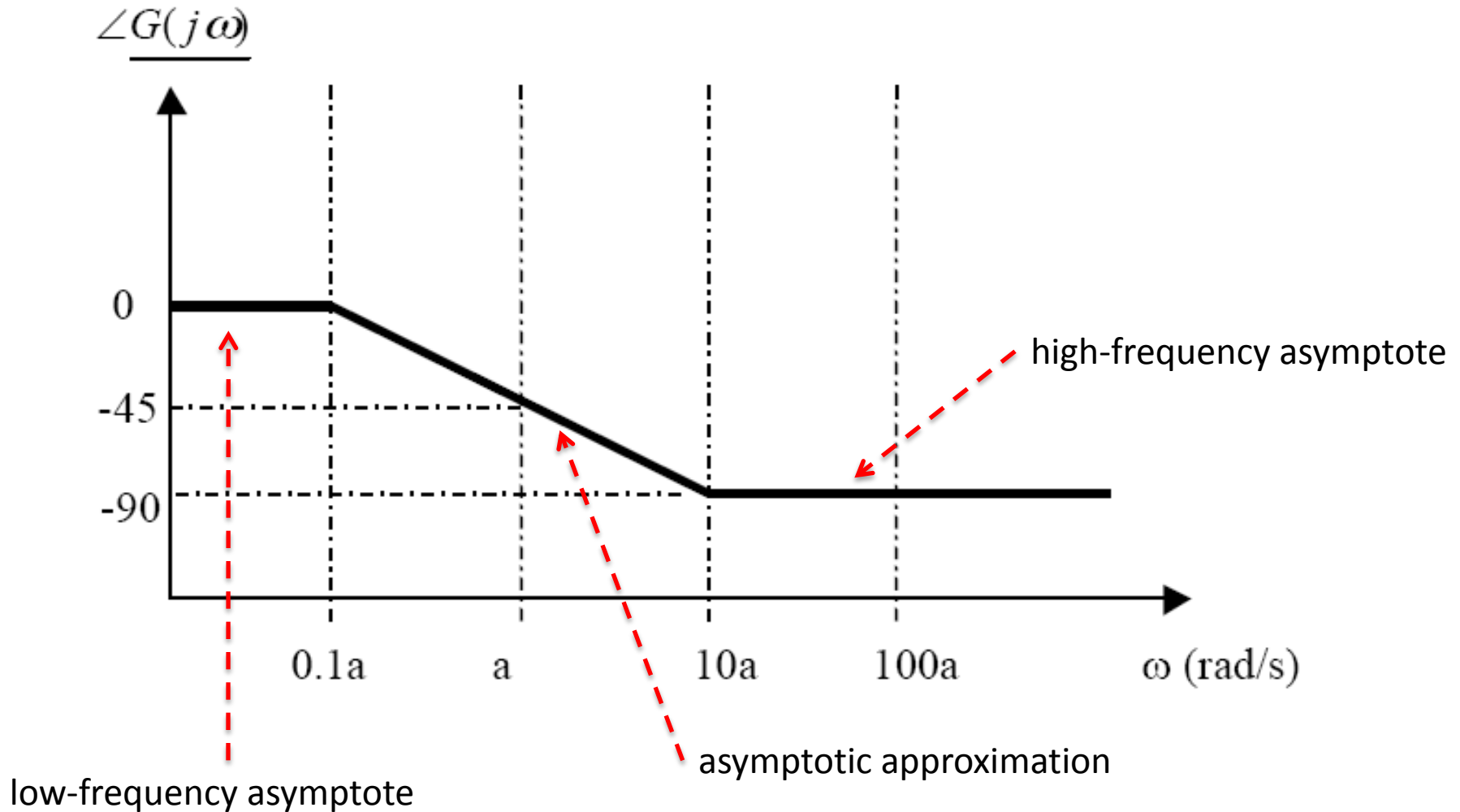
$$|G(j\omega)|_{dB} = 20 \log \frac{1}{\omega} \quad \text{- 20 dB/decade}$$

$$\angle G(j\omega) = -\tan^{-1} \omega = -90^0$$

## Bode Plots- Poles



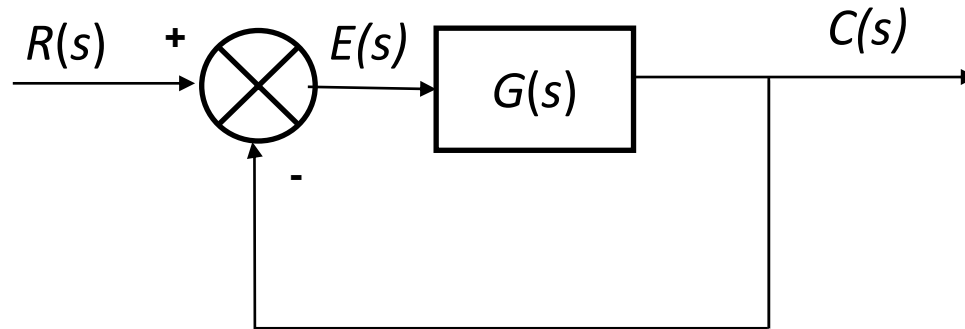
## Bode Plots- Poles



## Exercise 1

- Sketch the Bode plots for the system shown where

$$G(s) = \frac{K(s+3)}{s(s+1)(s+2)}$$



- Use the command in MATLAB to get the actual bode plot. (use the command 'bode(G)')

## Bode Plots: Second Order

- For

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

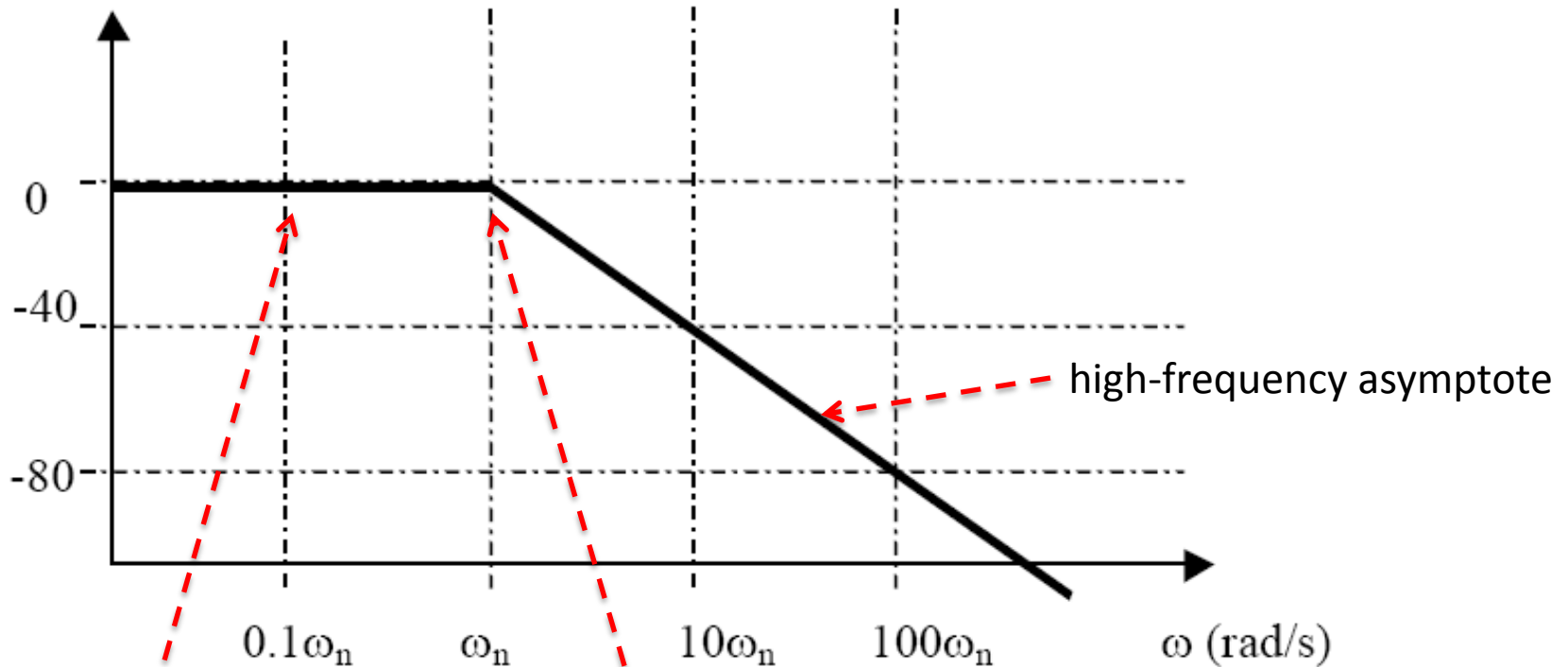
$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} = \frac{1}{\frac{s^2}{\omega_n^2} + \frac{2\zeta}{\omega_n} s + 1}$$

$$G(j\omega) = \frac{1}{\frac{(j\omega)^2}{\omega_n^2} + j\frac{2\zeta\omega}{\omega_n} + 1} = \frac{1}{\left(1 - \frac{\omega^2}{\omega_n^2}\right) + j\frac{2\zeta\omega}{\omega_n}}$$

- At low frequency,  $\omega \ll \omega_n$ ,  $G(j\omega) = 1$   
 $|G(j\omega)|_{dB} = 20\log 1 = 0 \text{ dB}; \angle G(j\omega) = 0^\circ$
- At high frequency,  $\omega \gg \omega_n$ ,  $G(j\omega) = 1/-\omega^2$   
 $|G(j\omega)|_{dB} = -20\log \omega^2 = -40\log \omega; \angle G(j\omega) = -180^\circ$



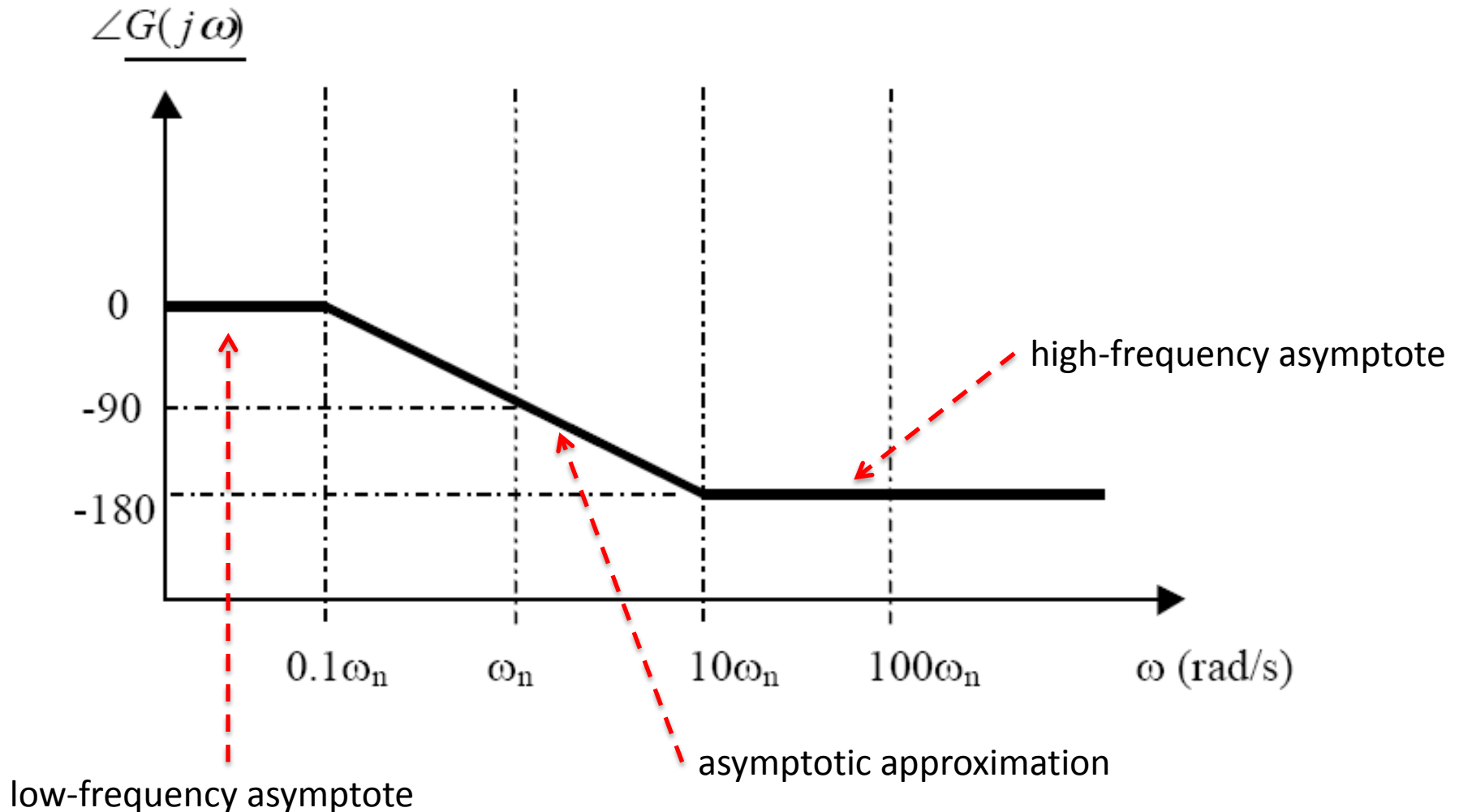
# Bode Plots: Second Order

 $|G(j\omega)| \text{ dB}$ 


low-frequency asymptote

break-frequency

## Bode Plots: Second Order



## Bode Plots: Second Order

$$G(s) = \frac{1}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

normalized

$$G(s) = \frac{1}{\frac{s^2}{W_n^2} + \frac{2Z}{W_n}s + 1}$$

$$G(jW) = \frac{1}{\frac{s^2}{W_n^2} + \frac{2Z}{W_n}s + 1} \Bigg|_{s \rightarrow jW}$$

At the break frequency,  $\omega = \omega_n$

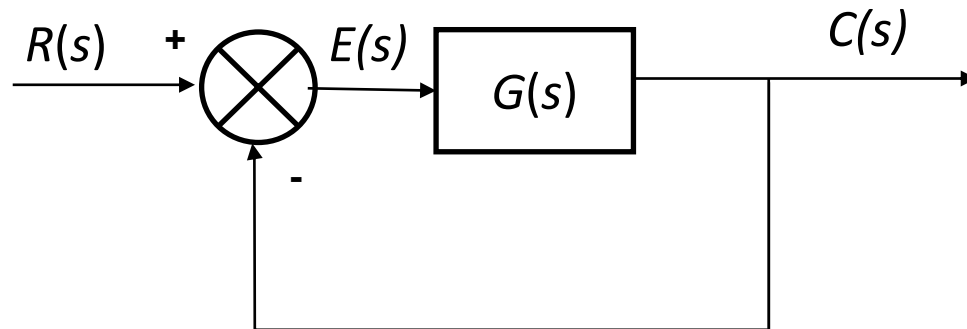
$$G(j\omega) = 1/j2\zeta$$

$$|G(j\omega)|_{dB} = -20\log(2\zeta); \angle G(j\omega) = -90^\circ$$

## Example 2

- Sketch the Bode plot for  $G(s)$  for the unity feedback system shown below where

$$G(s) = \frac{(s + 3)}{(s + 2)(s^2 + 2s + 25)}$$



Obtain the actual bode plot using MATLAB.

# 5.4

## Analysis of Bode Plot

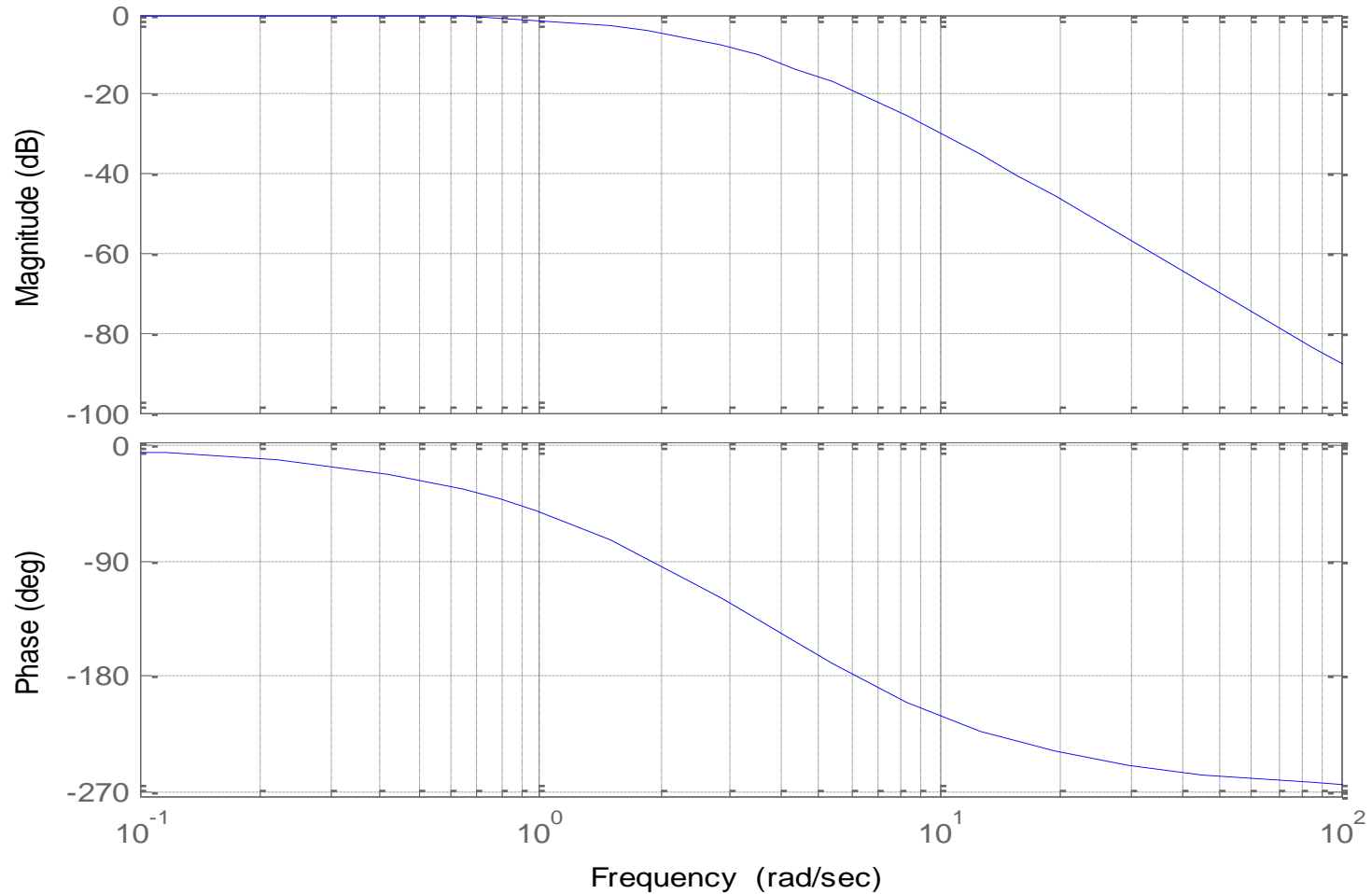
## Stability via Bode Plots

- Stability of a closed-loop system can be determined using Bode plot of an **open-loop system**.
- A closed-loop system is stable if the magnitude of the OL system is less than 0 dB (unity gain) at the frequency where the phase is  $\pm 180^\circ$ .
- **Example :**
- Use Matlab to get the actual plotting
- Determine the range of  $K$  within which the unity feedback system is stable. Let  $G(s) = K/[(s+2)(s+4)(s+5)]$ .
- Solution: Normalise

$$G(s) = \frac{K}{(40) \left(\frac{s}{2} + 1\right) \left(\frac{s}{4} + 1\right) \left(\frac{s}{5} + 1\right)}$$

- For convenience, choose  $K = 40$ .

## The bode plot when $K = 40$



## Solution 3

- With  $K = 40$ , at phase  $-180^\circ$ ,  $\omega = 7$  rad/s, magnitude = -20 dB.
- The system is stable at  $K = 40$ .
- Therefore, an increase in gain of 20 dB ( $20 \log 10$ ) is possible for stability.
- Hence the gain for stability is 400 ( $40 \times 10$ ).
- Range for stability:  $0 < K < 400$ .
- Actual results:  $\omega = 6.16$  rad/s,  $K = 378$ .

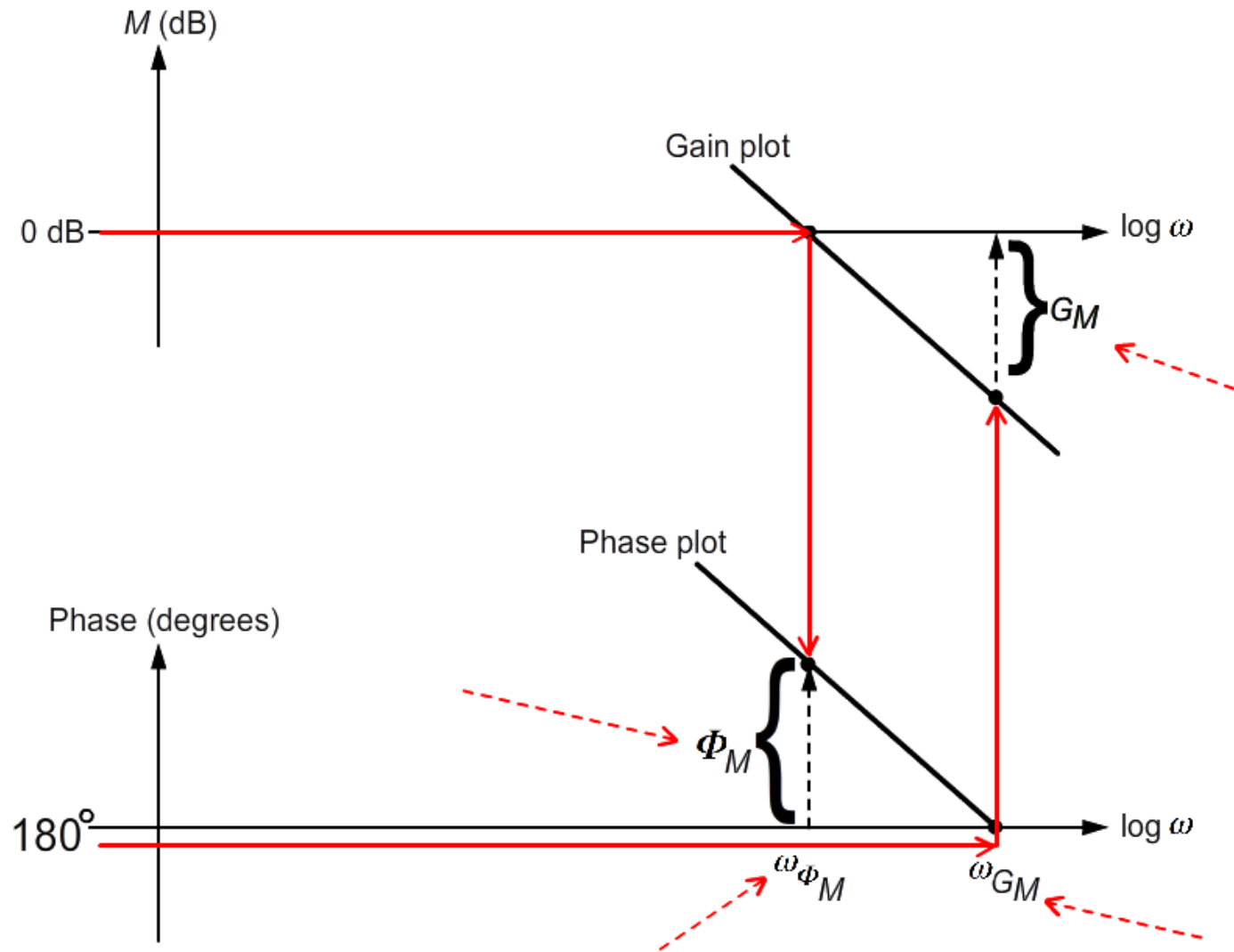


## Gain and Phase Margins

- Gain margin and phase margin are two quantitative measures of how stable a system is.
- Systems with greater gain and phase margins can withstand greater changes in system parameters before becoming unstable.
- **Gain margin,  $G_M$**  is the change required in open-loop gain at  $-180^\circ$  of phase shift to make the closed-loop system unstable.
- The gain margin is found by using the phase plot to find the gain margin frequency,  $\omega_{GM}$  where the phase angle is  $-180^\circ$ .
- At this frequency look at the magnitude plot to determine the gain margin which is the gain required to raise or decrease the magnitude curve to 0 dB.

- **Phase margin,  $\Phi_M$**  is the change required in open-loop phase shift to make the closed-loop system unstable.
- The phase margin is found by using the magnitude curve to find the phase margin frequency,  $\omega_{\Phi_M}$  where the gain is 0 dB.
- At this frequency, the phase margin is the difference between the phase value and  $-180^\circ$ .

# Gain and Phase Margins



## Example

Consider a unity feedback system :

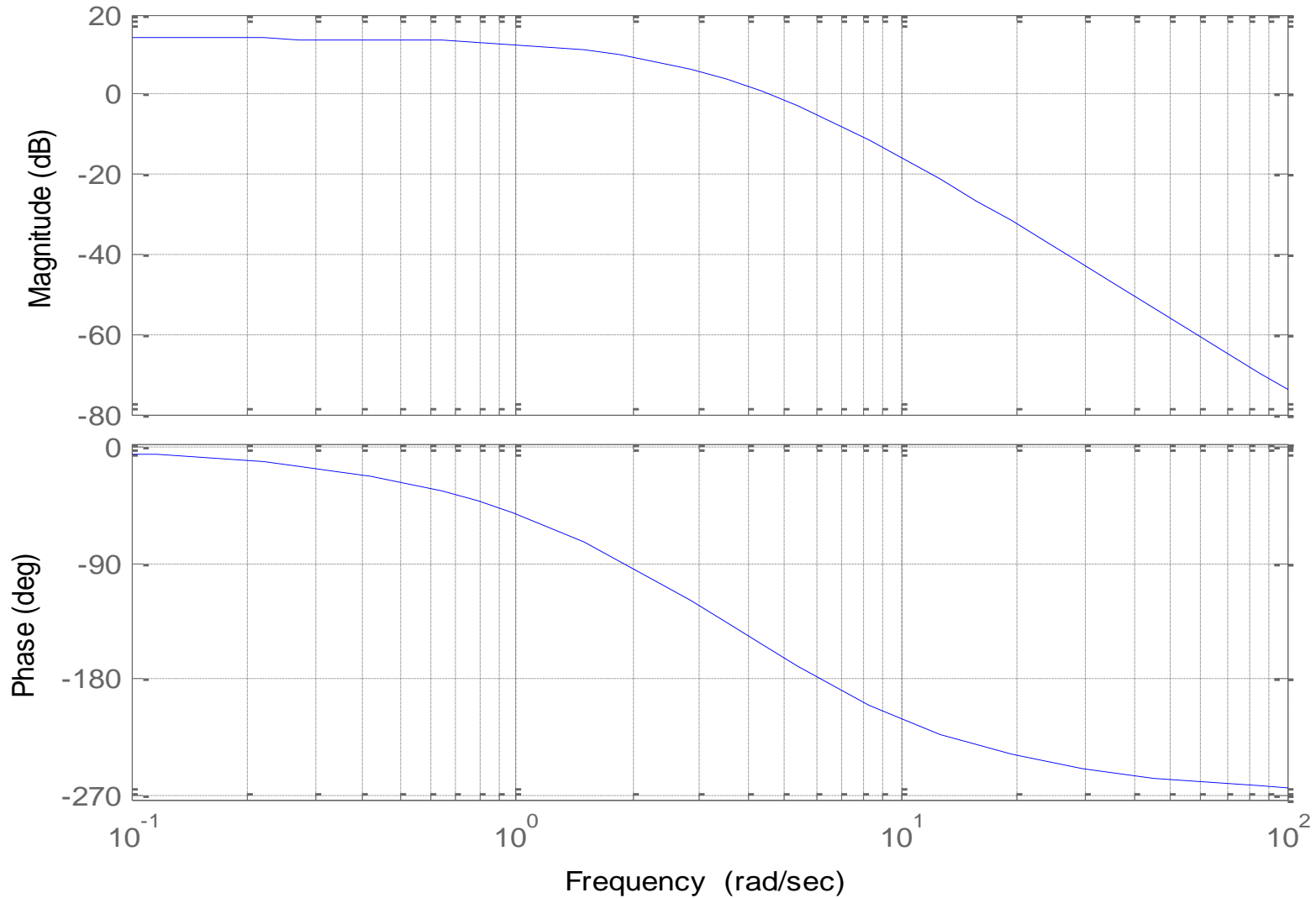
$$G(s) = 200/[(s+2)(s+4)(s+5)]$$

Using Matlab, find the gain margin and the phase margin from the bode plot.

### SOLUTION:

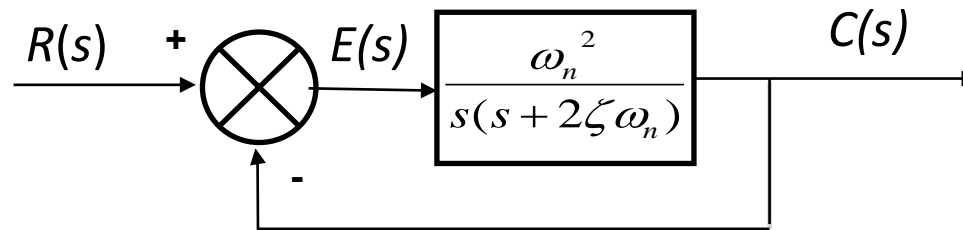
- $\omega_{GM} = 7 \text{ rad/s}$ .  $G_M = 6.02 \text{ dB}$ .
- $\omega_{\Phi_M} = 5.5 \text{ rad/s}$ .  $\Phi_M \text{ is } = 180^\circ - 165^\circ = 15^\circ$ .
- Note that: - any additional zeros and/or poles will change the original bode plot. This can be clearly observed by using the command 'sisotool(G)' and adding zeros/poles from the menu. Resulted in the changes in  $G_M$  and  $\Phi_M$ , hence the stability

Bode plot of the system :



# Relation between Closed-Loop Time and Closed-Loop Frequency Responses

- There is a relationship between closed-loop time and closed-loop frequency responses.
- Consider the second order feedback control system:



$$T(s) = \frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$T(j\omega) = \frac{\omega_n^2}{(j\omega)^2 + j2\zeta\omega_n\omega + \omega_n^2} = \frac{\omega_n^2}{(\omega_n^2 - \omega^2) + j2\zeta\omega_n\omega}$$

$$M = |T(j\omega)| = \frac{\omega_n^2}{\sqrt{(\omega_n^2 - \omega^2)^2 + 4\zeta^2\omega_n^2\omega^2}}$$

- By plotting the closed loop bode plot and looking at the magnitude-log plot, we can measure:
  - The maximum magnitude value of  $M_p$ ,

$$M_p = \frac{1}{2\zeta \sqrt{1-\zeta^2}}$$

- The frequency at the  $M_p$ ,

$$\omega_p = \omega_n \sqrt{1-2\zeta^2}$$

- Therefore, we can deduce that the maximum magnitude is directly related to damping ratio and overshoot of a system.

- Bandwidth,  $\omega_{BW}$  is the frequency at which the magnitude response curve is -3 dB.
- Relationships between the bandwidth and the time response specifications:

$$\omega_{BW} = \omega_n \sqrt{(1 - 2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2}}$$

$$\omega_{BW} = \frac{4}{T_s \zeta} \sqrt{(1 - 2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2}}$$

$$\omega_{BW} = \frac{\pi}{T_p \sqrt{1 - \zeta^2}} \sqrt{(1 - 2\zeta^2) + \sqrt{4\zeta^4 - 4\zeta^2}}$$



## Exercise 3

- Given a unity feedback system with  $G(s) = K/[s(s+1)(s+2)]$ . Using Matlab, find *the* system gain and phase margins, maximum amplitude and bandwidth for  $K = 1$  and 10.

### ANSWER

Gain and phase margins are obtained from the open-loop Bode plot. [prove using MATLAB]

Maximum amplitude and bandwidth can **only** be obtained with the closed-loop Bode plot. [prove using MATLAB]

	K = 1	K = 10
Gain margin	29.5 dB	9.5 dB
Phase margin	78°	25°
Maximum amplitude	0 dB	7.3 dB
Bandwidth	0.26 rad/s	2 rad/s

**Hard to find manually**

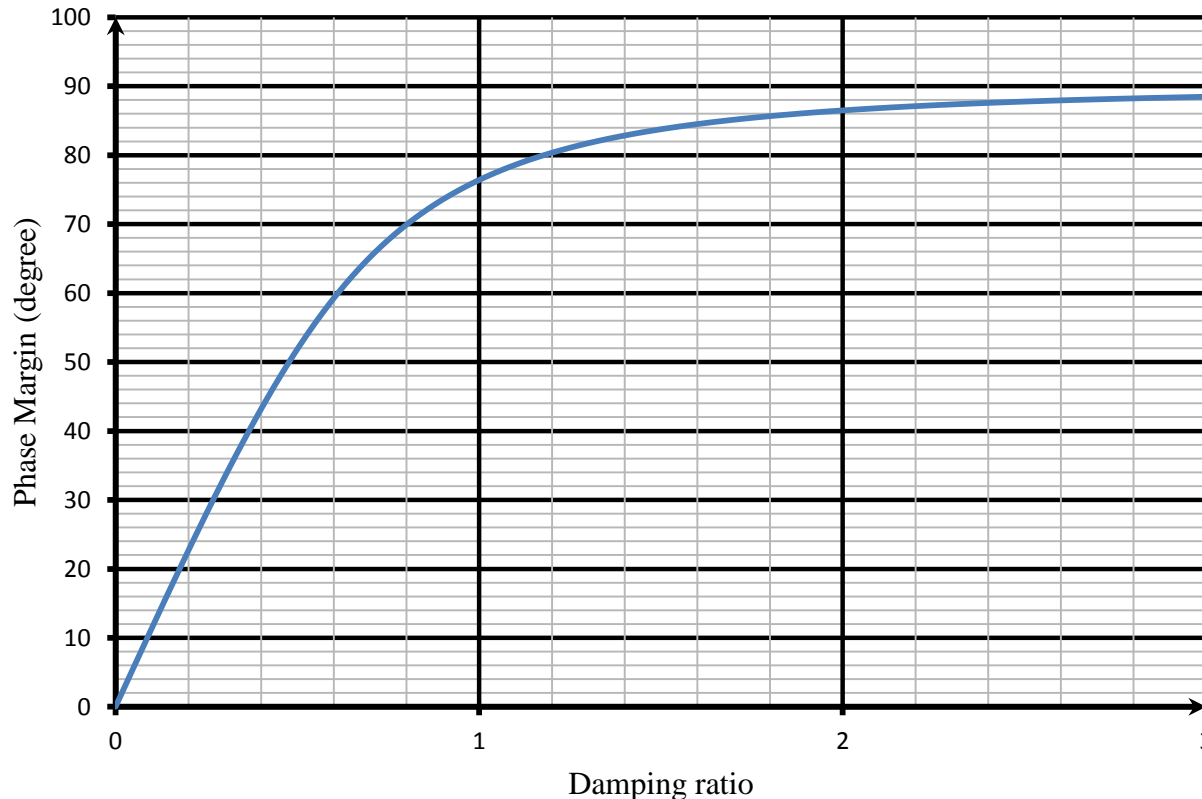
## Relation between Closed- and Open-Loop Frequency Responses

- We do not have an easy way of finding the closed-loop frequency response from which we could determine  $M_p$  and thus the transient response.
- We can sketch the open-loop frequency response (Bode plot) but not the closed-loop frequency response.
- One of the techniques to obtain the closed-loop frequency response from open-loop frequency response is **Nichols Chart** which is not covered in this module.

# Damping Ratio and Phase Margin

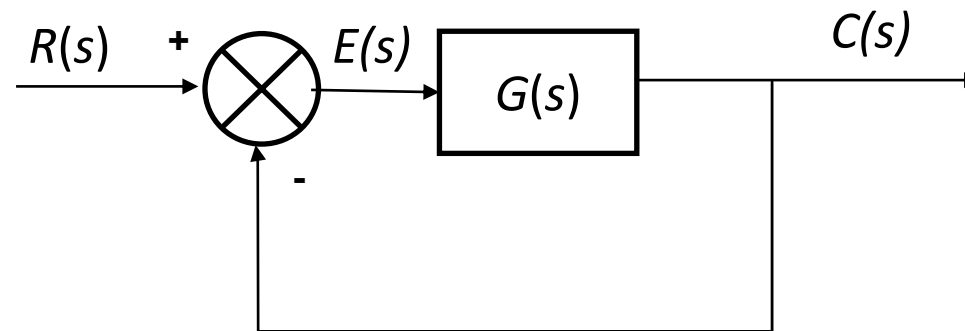
- The relationship between the phase margin and the damping ratio can be derived and given by:

$$\Phi_M = \tan^{-1} \frac{2\zeta}{\sqrt{-2\zeta^2 + \sqrt{1+4\zeta^4}}}$$



## Steady-state Error from Frequency Response

- The steady state error can also be found from the open loop bode plot and using the same formula from the time domain analysis
- For a unity feedback system, the steady state error can be further simplified.



$$e_{ss} = \lim_{s \rightarrow 0} \frac{sR(s)}{1 + G(s)}$$

- Hence, the static error constants are related to the input test signal.
- For a unit step input, the steady state error is given by,

$$\begin{aligned}
 e_{ss} &= \lim_{s \rightarrow 0} \frac{s}{1 + G(s)} \cdot \frac{1}{s} \\
 &= \frac{1}{1 + \lim_{s \rightarrow 0} G(s)} \\
 &= \frac{1}{1 + K_p}
 \end{aligned}$$

- where,  $K_p$  is the position error constant, given by

$$K_p = \lim_{s \rightarrow 0} G(s)$$

- For a unit ramp input, the steady state error is given by,

$$\begin{aligned}e_{ss} &= \lim_{s \rightarrow 0} \frac{s}{1 + G(s)} \cdot \frac{1}{s^2} \\ &= \lim_{s \rightarrow 0} \frac{1}{s + sG(s)} \\ &= \frac{1}{\lim_{s \rightarrow 0} sG(s)} \\ &= \frac{1}{K_v}\end{aligned}$$

- where,  $K_v$  is the velocity error constant, given by

$$K_v = \lim_{s \rightarrow 0} sG(s)$$

- For a parabola input, the steady state error is given by,

$$\begin{aligned}
 e_{ss} &= \lim_{s \rightarrow 0} \frac{s}{1 + G(s)} \cdot \frac{1}{s^3} \\
 &= \lim_{s \rightarrow 0} \frac{1}{s^2 + s^2 G(s)} \\
 &= \frac{1}{\lim_{s \rightarrow 0} s^2 G(s)} \\
 &= \frac{1}{K_a}
 \end{aligned}$$

- where,  $K_a$  is the velocity error constant, given by

$$K_a = \lim_{s \rightarrow 0} s^2 G(s)$$

## Steady-state Error from Frequency Response

- For a unity feedback system with an open-loop transfer function  $G(s)$ , the steady-state errors can be found identify the system type and using the respective formula:

- for system type 0: 
$$e_{ss} = \frac{1}{1 + K_p}$$

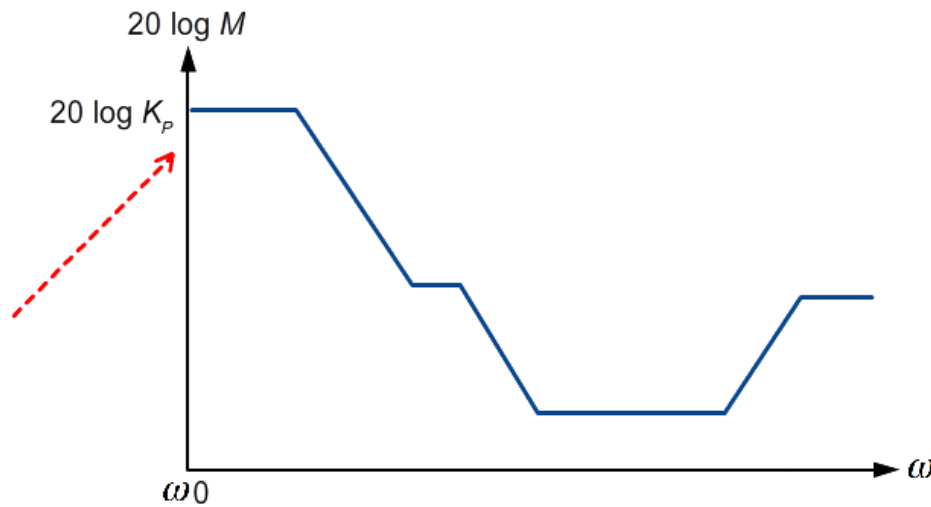
- for system type 1: 
$$e_{ss} = \frac{1}{K_v}$$

- for system type 2: 
$$e_{ss} = \frac{1}{K_a}$$

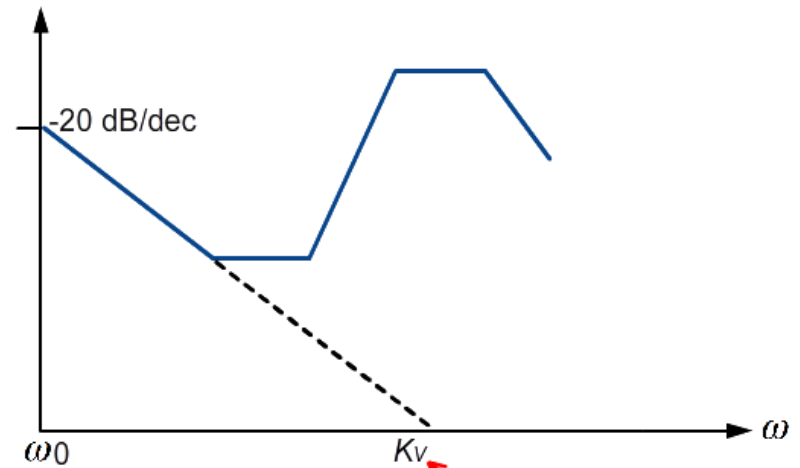


# Steady-state Error from Frequency Response

- By identifying the system type from the open-loop Bode plot, the steady state error can be easily found as follows,

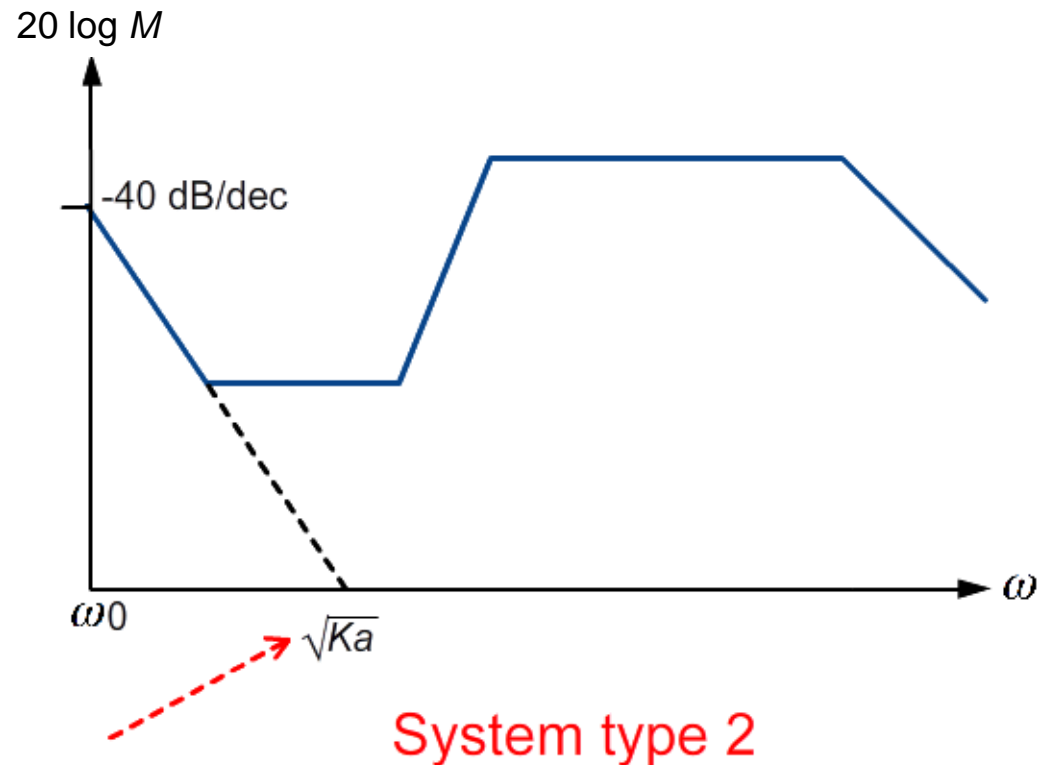


System type 0



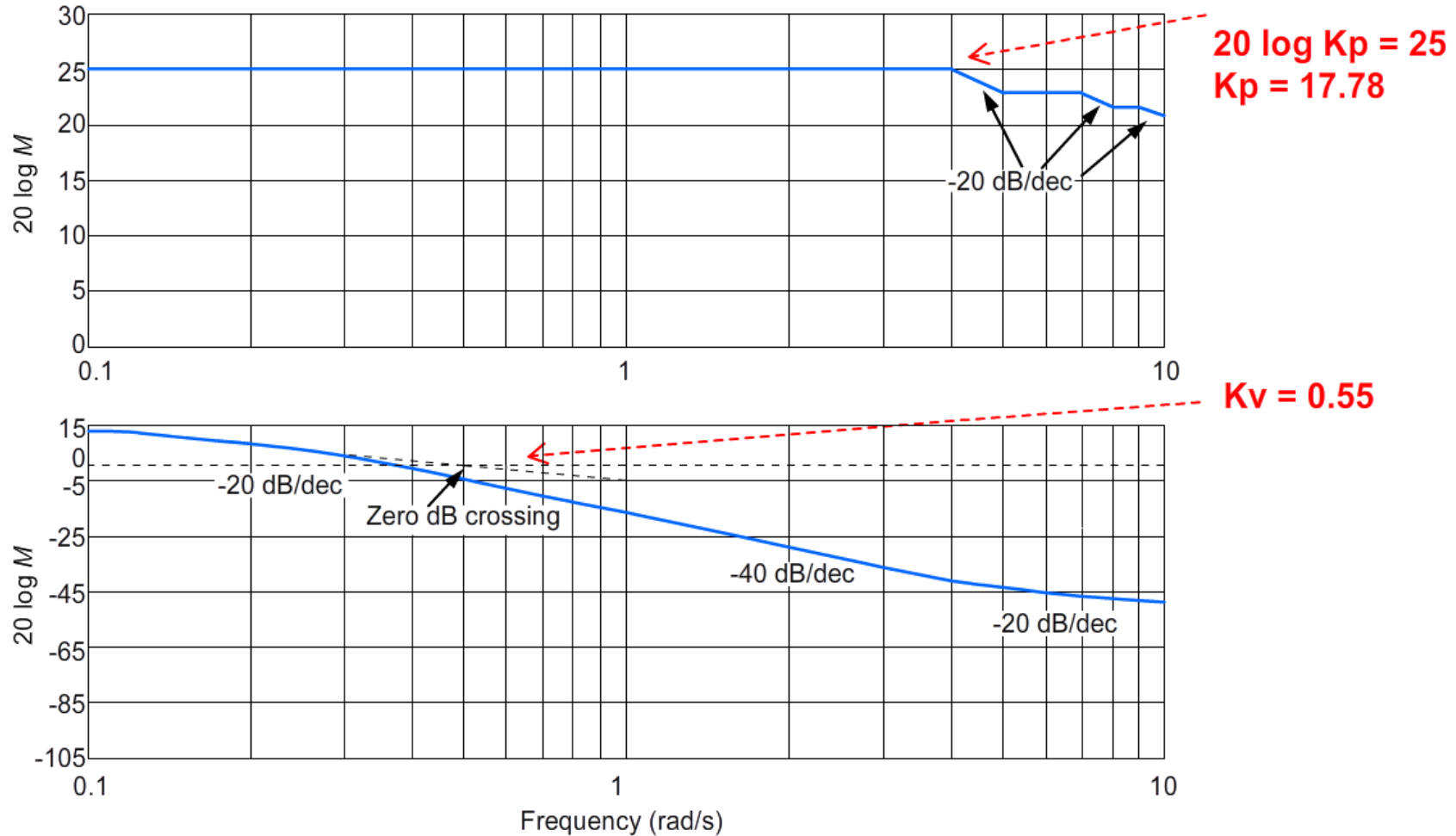
System type 1

# Steady-state Error from Frequency Response

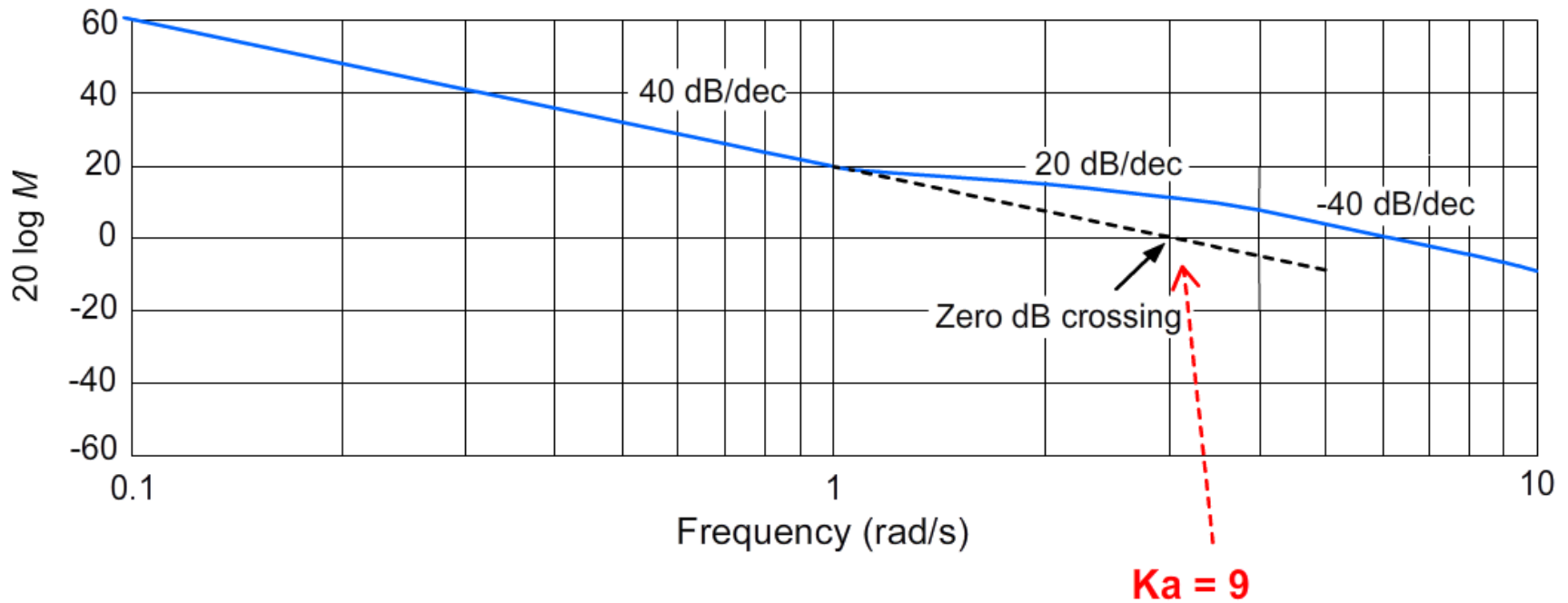


# Example

- Find the steady-state error for the following Bode plots:



# Example



# Conclusions

We have covered

- ✓ The graphical analysis using Bode Plot
- ✓ The stability analysis by looking at Gain and Phase Margins
- ✓ Some relationships between open loop and closed loop systems' information

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